Short story on how loading scenario influence failure of solid material under stretching

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History ...

2019, S. Pradhan, J.T. Kjelstadli, A. Hansen Variation of elastic energy shows reliable signal of upcoming catastrophic failure Frontiers in Phys., doi:10.3389/fphy.2019.00106 2021, W. Debski, S. Pradhan, A. Hansen **Criterion for Imminent Failure During Loading - Discrete Element** Method Analysis Frontiers in Phys., doi:10.3389/fphy.2021.675309



Fiber Bundle Model







Discrete Element Method (DEM)





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DEM simulations



Results (1)





Results (2)





Experimental confirmation

Damage evolution in specimens made with quasi-brittle materials: Experimental verification using Acoustic Emission technique

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ABSTRACT: Composites, both natural and engineered, present complex failure behaviour due to their heterogeneous nature. The localisation interaction among a cluster of micro-cracks and the size effect are some of the phenomena that govern the damage process. When dealing with systems composed of such materials, the Acoustic Emission (AE) technique is an excellent strategy to obtain information that allows us to understand and characterize the system's behaviour. The present work tested a pre-cracked prismatic basalt specimen until its complete fracture. The AE technique was employed, and the resulting signals were processed considering different acoustic emission global parameters endorsed in the specialized bibliography as precursors of the local/global collapse failure. Moreover, a measure of the temporal elastic energy derivative was computed from the data obtained in the experimental tests. The preliminary results showed that all of the obtained global evolution parameters performed well as failure precursors.



Experimental confirmation



Figure 4: Load vs. time, and derivative of elastic energy.

In Table 1, the times where the elastic energy derivative presents a local maximum were computed (t_n) , together with the moments where the local drops of the global load vs. time is registered (t_i) , and the ratio between the two values. (t_n/t_i) . From this table it is possible to see that the values of (t_n/t_i) doesn't change significantly. Debski et al. [1] discussed how (t_n/t_i) changes. This aspect will be further explored as a continuity of the present work.

Table 1: Collapse prediction time relationship with elastic energy delta.

	(a)	(b)	(c)	(d)	(e)
t _n [s]	137.44	157.59	219.23	273.91	280.31
t _i [s]	144.42	163.51	224.83	278.94	285.56
t_n/t_i [%]	95.17	96.38	97.51	98.20	98.16

Question:

What are limits of FBM/DEM?







what should we look for ?



Discrete Element Method

PP interactions
central forces
no internal PP-friction
bonds braking condition
geometry of the sample
internal structure of the sample

Fiber Bundle Model

- deals with deformation dynamics (x) onlymassless theory
- \star no kinetic energy (variation)
- \star no time evolution (no time scale)
- no space scale (only in ELS models)
- no thermodynamics (???)

What should we look for ?

no time scale

loading independence

DEM: search for dependences on loading velocity DEM: pay attention on kinetic energy variation **Perform simulation with different velocity** of moving plate !

Analysis of velocity dependences

- x_{min} extension when first PP bonds break
- x_{max} extension when sample splits off
- $E_p(x)$ total elastic energy
- $\Delta Nb(x)$ dynamics of bonds breaking

Begining of fracturing





Collaps of sample

Rupture duration 100 • 0 10 ••• Xmax 1 0.1 10 100 0.1 0.01 1 V [mm/s]



Elastic energy







Elastic energy



Broken bonds



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Partial conclusions

- apparently visible dependences on V
- high-, and low velocity breaking modes
- FBM appropriate for high velocity mode

















Nr = 2





Two breaking modes



"random"

"cooperative"

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Why











What about "precursor" at low V?





E1jVx4R2



Final conclusions

- high-, and low velocity breaking modes
- ✦ FBM appropriate for high velocity (???)
- more advanced DEM simulation model needed





